

5

Attorney Docket No. BVW014

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

10

* * * * *

APPLICATION FOR UNITED STATES LETTERS PATENT15
15**TITLE OF THE INVENTION:**

Blow-molding Large, Relatively Thick-walled, Thermoplastic Resin Products.

CROSS-REFERENCES:

None.

20

FIELD OF THE INVENTION:

The present invention relates generally to the manufacture of large, relatively thick-walled, blow-molded, thermoplastic-resin products, and particularly concerns both methods and apparatus for accomplishing the separation of gutter flash that is first integrally attached to a large, relatively thick-walled, blow-molded product from the product entirely around the product mold-line perimeter while the product is fully restrained in the product-forming mold cavity of the invention apparatus.

BACKGROUND OF THE INVENTION:

It is common practice in the United States in connection with the manufacture of large, relatively thick-walled blow-molded thermoplastic resin products using conventional production blow-molding machines and known blow-mold assemblies to eject the molded product with simultaneously formed and completely surrounding gutter flash from the mold assembly, and to afterwards completely separate the integrally attached flash from the ejected blow-molded product by subsequent combined operations such as sequential cutting and grinding or sequential shearing and grinding. The operating forces and processing time required to so-separate and remove such flash, either manually or by machine, are, in the case of many blow-molded products, extremely large. The required flash separation forces and flash removal process times are especially substantial in cases where the blow-molding machine production cycle unit output is comprised of either a single blow-molded product or multiple blow-molded products with integrally attached gutter flash having a substantial total length of gutter flash trim edge.

In the teachings of U.S. Patent No. 5,480,607 granted to Hobson a method of separating integrally attached flash from a product during the molding process is disclosed, but such method utilizes a step wherein the flash is temporarily secured to the apparatus blow-mold and the formed product is separated from the restrained integral flash by applying product mold ejector pin forces to the blow-molded product with the mold assembly in a partially open condition. The ejection forces required may be undesirably large and also generally cause ejector pin damage to the formed product in high-rate production cycles wherein the blow-molded product has an elevated temperature and a substantial degree of residual parison plasticity at time of flash separation and product ejection from its mold.

I have discovered a novel method of progressively separating integrally-attached gutter flash from a blow-molded product, and also novel mold assembly constructions and methods of assembly operation, that may be used in conjunction with a conventional production blow-molding machine to achieve complete, or very nearly complete, separation of otherwise integrally attached surrounding gutter flash from blow-molded products while the products are fully restrained by the mold apparatus and prior to product ejection from within the mold apparatus. Subsequently the individual blow-molded thermoplastic resin products and separated gutter flash are ejected from the mold assemblies in which they were formed and removed from the co-operating conventional production blow-molding machine. Because very short blow-molding machine operating cycle unit times may be achieved with the novel in-mold product de-flashing, and because the apparatus takes advantage of separate product and gutter flash removal procedures, the blow-molded thermoplastic resin products and separate gutter flash have no possibility of being inadvertently fused together.

In addition, when it has been discovered that the wall thickness configuration characteristic of the produced blow-molded product in the region of the product mold parting-line perimeter is not that which is desired, e.g. is convex or of uniform wall thickness rather than concave, is concave or of uniform wall thickness rather than convex, etc., it has been necessary and costly to rather extensively re-work the blow-mold assembly to obtain correction to the desired product wall thickness configuration at the product mold parting line perimeter. I have found that the required rather extensive blow-mold assembly re-working is not necessary if using the improved blow-mold apparatus of the present invention.

Other objects and advantages of the present invention will become apparent during consideration of the detailed descriptions, drawings, and claims which follow.

SUMMARY OF THE INVENTION:

I have invented a blow-mold assembly that is intended for use with a conventional production blow-molding machine and that is comprised of co-operating and separable cap and base blow-mold sub-assemblies, the base blow-mold sub-assembly having multiple elongated gutter plate segments 5 which together surround the blow-mold assembly product mold cavity when abutted, which each may be moved linearly in directions toward or away from the cap blow-mold sub-assembly to obtain different product wall thickness and internal surface configuration characteristics at the product mold parting-line perimeter, and which also are pivoted or rotated in directions transverse to the direction of linear gutter plate segment movement to progressively separate gutter flash from around the blow-molded product while the product is retained in the apparatus product mold cavity. Further, the 10 blow-mold assembly invention, with modification, is useful for additionally separating from the product a gutter flash core integrally attached to the product at a product interior mold parting-line perimeter also while the product is retained in the apparatus product mold cavity.

Several different blow-mold assembly embodiments and methods of blow-molding a product 15 for implementing the invention are disclosed and described in detail.

BRIEF DESCRIPTION OF THE DRAWINGS:

Figure 1 is a schematic perspective view of a conventional production blow-molding machine within which the methods and apparatus of the present invention may be practiced;

20 Figure 2 is a schematic elevation view of the interior of the blow-molding machine of Figure 1 illustrating a preferred embodiment the base and cap blow-mold sub-assemblies of the present invention in an operationally separated condition;

Figure 3 is similar to Figure 2 except that the included invention cap and base blow-mold sub-assemblies are illustrated in an operationally closed condition;

Figure 4 is similar to Figure 3 except that it is a plan view of the interior of the blow-molding machine of Figure 1 illustrating the blow-mold sub-assemblies of the present invention in a
5 fully closed condition;

Figure 5 is an orthogonal view of the invention base blow-mold sub-assembly shown in Figures 2 through 4 in an initial operating condition;

Figure 6 is an orthogonal view of the invention base blow-mold sub-assembly similar to Figure 3 but in a subsequent operating condition;

Figure 7 is a section view taken at line 7-7 of Figure 3 in an invention blow-mold assembly initial operating condition;

Figure 8 is a view similar to Figure 7 but in an invention blow-mold assembly subsequent operating condition;

Figure 9 is an enlarged view of the portion of Figure 7 circled with a dotted line;

15 Figure 10 is an enlarged view of the portion of Figure 8 circled with a dotted line;

Figure 11 is a section view taken at line 11-11 of Figure 13;

Figure 12 is a schematic plan view of the product that is blow-molded in the apparatus of Figures 1 through 11 and its fully-separated gutter flash;

Figure 13 is a schematic front elevation view of the invention Figure 5 base blow-mold sub-assembly but with the gutter plate segments surrounding the mold cavity having an alternate
20 configuration;

Figure 14 is a schematic diagram of one form of control system that may be utilized to obtain proper sequencing of the several bi-directional actuator devices incorporated in the apparatus of Figures 1 through 11;

Figures 15 through 17 are section views similar to Figure 9 but illustrating the different 5 product parting line perimeter wall thickness or wall internal surface characteristics that can be obtained by practice of the present invention;

Figure 18 is an orthogonal view of another embodiment of the invention base blow-mold sub-assembly shown in an initial operating condition;

Figure 19 is an orthogonal view of the invention base blow-mold sub-assembly of Figure 18 in a subsequent operating condition;

Figure 20 is a schematic section view taken at line 20-20 of Figure 18;

Figure 21 is a schematic section view taken at line 21-21 of Figure 18 to illustrate included 10 gutter flash ejector pin elements in a retracted operating condition;

Figure 22 is similar to Figure 21 but illustrating the included gutter flash ejector pin elements 15 in a subsequent extended operating condition;

Figure 23 is an elevation view illustrating the molded part and gutter flash components that are ejected from the blow-molding machine of Figures 1 through 4 when utilizing the base blow-mold sub-assembly of Figures 18 and 19;

Figure 24 is an schematic orthogonal view of still another embodiment of the invention base 20 blow-mold sub-assembly in an initial operating condition;

Figure 25 is a schematic section view taken at line 25-25 of Figure 24 to illustrate included invention internal crash pad elements in an extended operating condition;

Figure 26 is similar to Figure 25 but illustrating the included crash pad elements in a retracted operating condition;

Figure 27 is a schematic section view taken at line 27-27 of Figure 24 to illustrate included gutter plate segment support pin elements in a first operating condition;

5 Figure 28 is similar to Figure 27 but illustrating the included gutter plate support pin elements in a different operating condition;

Figures 29 and 30 schematically and orthogonally respectively illustrate additional cap blow-mold sub-assembly and base blow-mold sub-assembly constructions that may be utilized in another application for the invention apparatus using the blow-molding machine of Figures 1 through 4;

10 Figure 31 is a section view illustrating the blow-mold sub-assemblies of Figures 29 and 30 in an assembled and first operating condition;

Figure 32 is a section view similar to Figure 31 but illustrating the sub-assemblies in a second operating condition;

Figure 33 is an enlarged view of the portion of Figure 32 circled with a dotted line;

15 Figure 34 is a schematic orthogonal view of yet another embodiment of the base blow-mold sub-assembly of the present invention;

Figure 35 is a section view through the invention blow-mold assembly taken, with blow-molded product in place, at line 35-35 of Figure 34;

20 Figure 36 is a plan view of the product mold half included in the base blow-mold sub-assembly of Figure 34;

Figure 37 is a section view taken at line 37-37 of Figure 34;

Figure 38 is a schematic front elevation view of another embodiment of the base blow-mold sub-assembly of the present invention with the included elongate and double-pivoted gutter plate segments in an initial operating condition;

5 Figure 39 is a view similar to Figure 38 but illustrating the included elongate and double-pivoted gutter plate segments in a subsequent operating condition;

Figure 40 is a back elevation view schematically illustrating a first embodiment of the of the Figures 38 and 39 base blow-mold sub-assembly gutter plate segment drive;

Figure 41 is similar to Figure 40 but schematically illustrating a second or different embodiment of the Figures 38 and 39 base blow-mold sub-assembly gutter plate segment drive;

Figure 42 is a partial break-away orthogonal view of the base blow-mold sub-assembly corner area construction utilized in invention embodiments of Figures 38 through 41;

Figure 43 is a schematic front elevation view of a base blow-mold sub-assembly construction for use in effecting progressive separation of an integrally attached gutter flash interior core from a blow-molded product, and illustrated in an initial operating condition;

15 Figure 44 is similar to Figure 43 but illustrating the blow-mold sub-assembly in a subsequent operating condition;

Figure 45 is a back elevation view schematically illustrating a first embodiment of the of the Figures 43 and 44 base blow-mold sub-assembly gutter plate segment drive;

Figure 46 is a section view taken at line 46-46 of Figure 43; and

20 Figure 47 is a section view taken at line 47-47 of Figure 44.

Machine 10 typically includes the illustrated feedstock hopper 12, a feed screw feedstock conveyor 14, and a conventional melter-accumulator-extruder sub-assembly 16 with variably-controlled parison die head 18. Machine 10 also includes guideposts 19 upon which movable platens 20 and 24 reciprocate. Movable machine platen 20 carries base blow-mold sub-assembly 22 and 5 movable machine platen 24 carries cap blow-mold sub-assembly 26. Although such base and cap blow-mold sub-assemblies have co-operating complementary product-forming cavities and generally similar constructions, their respective total function differs.

Machine platen 20 is powered by bi-directional rapid traverse hydraulic actuator 28 and 10 additionally by bi-directional clamping hydraulic actuators 32 and 34; machine platen 24 is powered by bi-directional rapid traverse hydraulic actuator 30 and additionally by bi-directional clamping hydraulic actuators 36 and 38. In addition, conventional blow-molding machine 10 typically includes trimmed blow-mold product discharge conveyor 42, flash discharge conveyor 44, and may optionally also include a conventional overhead discharge conveyor 46 (see Figure 1) normally utilized for removing conventionally formed product units with integrally attached flash from within the machine. 15 Machine 10 typically also includes a operator's control panel or control station 48 and access doors 50 which, when opened, provide access to the interiorly-located invention blow-mold sub-assemblies 22 and 26 for installation and maintenance servicing purposes and the like.

As shown in Figures 4 and 5, base mold sub-assembly 22 is provided with a base plate 60 to 20 which are rigidly attached slotted platen mounting blocks 62 and 64, intermediate support block 66, and external crash pads 68 and 70 which function to maintain a proper base blow-mold sub-assembly distance of separation from cap blow-mold sub-assembly 26 when such blow-mold sub-assemblies are positioned in an operationally closed condition with respect to each other, usually a small distance

generally not exceeding approximately ten thousandths (0.010) of an inch and often to as little as approximately one thousandth (0.001) of an inch, the separation in that range utilized in a particular apparatus blow-mold assembly being controlled in some instances by the selection and installation of multiple sets of different hereinafter-described shim combinations. Also, this separation distance may

5 increase somewhat both when pressurized air is being injected into the interior of the parison segment constrained by the mold sub-assemblies during product formation, and also after the actuators forcing the mold sub-assemblies together are relieved of internal fluid pressures prior to opening the mold sub-assemblies for product and gutter flash removal purposes. Crash pads 70 each have a projecting tapered guide pin 72 that co-operates with a complementary crash pad tapered guide pin receptacle

10 74 provided in a crash pad element 68.

Base blow-mold sub-assembly 22 also includes product mold half 80 that is rigidly mounted on base plate 60, and that has a product cavity half 82, pneumatically-actuated conventional bi-directional product ejectors 84, and a pneumatically-actuated extendible and retractable inflation needle 86 that injects pressurized air into the interior of parison 40 to effect parison expansion.

15 Elongate gutter plate segments 90, 92, 94, and 96, together surround cavity 82 of product mold half 80 at the cavity mold parting-line perimeter when their ends each abut the ends of an adjacent gutter plate segment . The essentially flat surface of each such gutter plate segment that opposes and is nearest cap blow-mold sub-assembly 26 is a gutter flash clamping surface designated in the drawings with the reference numeral 87, and includes an excess gutter flash receiver 98 which in Figures 5

20 through 13 takes the form of multiple, excess gutter flash, tapered blind-hole recesses. As discussed in connection with Figures 15 through 17, each such receiver element 98 is provided for the purpose of accommodating excess heated parison material associated with the particular distance that

separates the gutter flash clamping surface **83** of cap blow-mold sub-assembly **26** from the gutter flash clamping surfaces **87** of the sub-assembly **22** pivoted gutter plate segments. Also, each such gutter plate segment included in mold sub-assembly **22** preferably includes multiple, conventional, bi-directionally and pneumatically-actuated gutter flash ejectors **100**, a longitudinal coolant passageway **102**, and an upstanding integral gutter flash separation blade element **97** positioned transversely at one or at each extreme end region of each elongated gutter plate segment. See Figure 11. Blade element **97** substantially cuts through said gutter flash to enable said gutter plate segments **90**, **92**, **94**, and **96** to pivot and progressively tear said gutter flash.

110 80 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99

Cap blow-mold sub-assembly **26**, although constructed to be generally similar to base blow-mold sub-assembly **22** with respect to its basic components, has a somewhat different total function than does its co-operating base blow-mold sub-assembly **22**. The cap blow-mold sub-assembly's mold half, which is designated **81** in Figures 5 through 10 and which together with co-operating product mold half **80** comprises the apparatus product mold with an interior product-forming cavity **82**, has an integral gutter with gutter flash clamping surface **83** which completely surrounds the product cavity periphery areas situated opposite the gutter flash clamping surfaces **87** of gutter plate segments **90** through **96**. Such cap blow-mold sub-assembly flat gutter flash clamping surface **83** also preferably diverges away from the gutter flash clamping surfaces **87** of the gutter plate segments of base blow-mold sub-assembly **22** outwardly from the product cavity mold parting-line perimeter **108**. The resulting "taper" is preferably at least about a 1° angular departure, sometimes is imparted to a flat continuous gutter flash clamping surface **83**, but optionally and often preferably, may advantageously includes an intermediate step or offset **85** located outwardly of mold parting-line perimeter **108** - usually about 3/4 inch from the parting-line perimeter, and just outwardly of the

position of concave excess gutter flash receiver or cleat 98 or its elements provided in the different invention gutter plate segment configurations. See Figure 10. Also, since blow-mold sub-assembly 26 does not support any of the invention pivoted and abutting gutter plate segments it is not provided with bi-directional hydraulic actuators for effecting pivotal movement of the invention gutter plate segments. While it is important that each gutter plate segment of sub-assembly 22 is provided with a longitudinal cooling water passageway 102 that is connected to a flowing source of liquid coolant such as cooling water, it is also important that product mold halves 80 and 81 of blow-mold subassemblies 22 and 26 each be provided with interconnected cooling water passageways 106 that are situated in the region of the product mold parting-line perimeter 108 and that are connected to a source of flowing coolant. In some applications the coolant may have a solidification temperature significantly lower than the solidification temperature of water, i.e. significantly lower than 32° Fahrenheit. See Figures 7 through 10 for illustration of the location of coolant passageways in proximity to the mold parting-aline perimeter 108.

It should be noted that each end-abutting and double-pivoted gutter plate segment 90, 92, 94 and 96 utilized in the practice of my invention is provided with two pivot axes, each such pivot axis having a longitudinal axis that is transverse (at right angles) to the plane of the product cavity mold parting-line perimeter and that is positioned at or in a different one of the end regions or opposite extremes of the elongated gutter plate segment. In some invention embodiments both pivot axes are movable in directions lying in the plane of the product cavity mold parting-line perimeter. In other invention embodiments, only one such pivot axis of a gutter plate segment is movable relative to the product cavity mold parting-line perimeter, while the other such pivot axis is maintained in a relatively fixed position. The movable pivot axes are moved (powered) by a co-operating bi-directional

actuator, and extension and retraction of the actuator piston rod causes the connected gutter plate segment to be rotated about or relative to each of its pivot axes.

Base blow-mold sub-assembly **22** includes a gutter plate segment drive which in the Figures 5 and 6 embodiment is comprised of bi-directional hydraulic actuators **110** through **124** that are each rigidly mounted on structure of sub-assembly **22** and, as shown in detail, the piston rod free end of each such actuator is connected to its respective end region of the adjacent gutter plate segment **90**, **92**, **94** and **96** by a pivot connection **126** that includes its respective gutter plate segment pivot axis.

Each such pivot connection preferably is designed to permit the attached gutter plate segment to:

(1) primarily be rotated about the pivot axis of the pivot connection for purposes of effecting progressive gutter flash separation from the blow-molded product while the product is fully retained within the assembly product cavity, and (2) secondarily be translated in directions parallel to the pivot axis of the pivot connection for purposes of establishing the desired product wall thickness configuration at the product mold parting line perimeter **108**. See Figures 7 through 10 and the discussion of Figures 15 through 17. A different number of thin shims **128** may be inserted under each bronze wear bushing **130** that supports a gutter plate segment underside bronze wear surface **132**, or alternatively, the bronze wear bushings may be extended or retracted using the actuating mechanism discussed in connection with the apparatus particulars of Figures 27 and 28. Pivot connections **126** enable the pair of bi-directional hydraulic actuators connected to the opposite or extreme ends of an invention elongated gutter plate segment **90**, **92**, **94** and **96** having two movable pivot axis to be actuated differentially to effect the progressive separation of integrally attached gutter flash from product **P** along the product mold parting-line perimeter **108**. adjacent the gutter plate segment.

Also, and while not shown in the drawings or suggested elsewhere, other primary power sources such as electric motors combined with various mechanical linkages, devices, and the like may be substituted for bi-directional actuator components 110 through 124 and utilized as the actuators that cause movement of gutter plate segments 90 through 96 relative to the co-operating product 5 molds.

1000 800 600 400 200 100 50

In Figure 13 I illustrate, in elevation, the gutter plate segment gutter flash clamping surfaces of invention blow-mold assembly 22 as having a different arrangement of tapered, blind- hole recesses that comprise excess gutter flash receiver elements 98 in comparison to the arrangement of Figures 5 and 6. Since the descending and superimposed heated tubular parison 40 illustrated in Figure 13 has programmed sections or zones of reduced thickness 40a and of increased thickness 40b to meet product wall thickness needs, I find it preferable to have added excess gutter flash receiver element 98 capacity in the adjacently situated zones of the gutter plate segments 90, 92, 94, and 96 that surround the product cavity of apparatus product mold half 80 rather than increased receiver element depth. Basically, I strive to have an extent of receiver element surface area or volume 15 provided in the gutter plate segments that generally is directly proportional to the volume (i.e., wall thickness) of thermoplastic resin material in the adjacent zones or sections of the descended heated parison. Figure 14 schematically illustrates one type of control system that may be utilized in connection with combined blow-mold sub-assemblies 22 and 26 to obtain proper sequencing of the different incorporated pneumatic/hydraulic bi-directional actuators in order to carry out the basic 20 product de-flashing steps of my method invention for the product application of Figures 1 through 13. Such control system preferably includes a compressed air source 150, a pressurized hydraulic fluid supply 152 with fluid reservoir 154, and a conventional programmable valve position sequence

controller 156 that sequentially activates each of the included conventional 4-way fluid valves 158 to its different valve operating positions and thereby achieve full extension or full retraction of each of the specifically numbered bi-directional actuators connected thereto at the proper time in each production cycle of blow-molding machine 10.

5 The basic sequence of steps for operating blow-molding machine or system 10, including blow-mold sub-assemblies 22 and 26, for a complete machine production cycle are as follows:

1. Activate machine 10.
2. Retract platens 20 and 24 to fully-separate (open) blow-mold sub-assemblies 22 and 26 (machine function).
3. Cause heated tubular thermoplastic resin parison 40 to descend from die-head 18 to lower edges of assemblies 22 and 26 (machine function).
4. Rapid advance platens 20 and 24 sufficient to engage all crash pads 68 and 70 and thereby fully close blow-mold sub-assemblies 22 and 26 by actuating rapid traverse hydraulic actuators 28 and 30 (machine function).
5. Clamp blow-mold sub-assemblies 22 and 26 together by simultaneously activating hydraulic actuators 32, 34, 36, and 38 (machine function) to engage and contact fully gutter plate segments 90 through 96 with the gutter flash F, and to flow excess thermoplastic resin parison material into surface reservoirs 98, whereupon accelerated cooling of parison gutter flash material commences.
6. Insert inflation needles 86 into the descended parison contained within mold assemblies 22 and 26.
7. Inject compressed air into contained parison thereby expanding heated parison

thermoplastic resin into complete contact with the product cavities **82** of blow-mold sub-assemblies **22** and **26** (machine function) and form thermoplastic resin product **P**.

8. Activate (retract) bi-directional hydraulic actuators **110**, **114**, **118**, and **122** to pivot gutter plate segments **90**, **92**, **94**, and **96**, respectively, thereby separating gutter flash **F** from blow-molded product **P** progressively along the product mold parting line perimeter using tension forces.

5

9. Complete gutter flash separation by activating (retracting) bi-directional hydraulic actuators **112**, **116**, **120**, and **124** to additionally pivot ("rock") gutter plate segments **90**, **92**, **94**, and **96**, respectively, but in an opposite rotational sense to thereby complete separation of gutter flash **F** from blow-molded product **P** progressively along the product mold parting-line perimeter using tension forces.

10. Reverse the actuation of clamping bi-directional hydraulic actuators **32**, **34**, **36**, and **38** (machine function) to release mold assembly clamping pressures.

15

11. Reverse the actuation direction of bi-directional rapid traverse hydraulic actuator **30** to partially separate and open blow-mold assemblies **22** and **26**.

12. Actuate pneumatic bi-directional gutter flash ejectors **100** to separate gutter flash segments **F** from engagement with the gutter plate segments **90**, **92**, **94**, and **96** of blow-mold sub-assembly **22** for free-fall to the machine flash removal conveyor **44**.

20

13. Reverse the actuation direction of bi-directional rapid traverse hydraulic actuator

28 to fully separate and open blow-mold sub-assemblies 22 and 26.

14. Actuate product ejectors 84 to release product units P from product mold cavities 82 for free-fall to the machine product removal conveyor 42.
15. Extend bi-directional hydraulic actuators 110 through 124 to return gutter plate segments 90, 92, 94, and 96 to their initial position abutting assembly mold 80.

16. Repeat steps 3 through 15 to end of machine production run.

Other arrangements for sequencing the actuation of gutter plate segments 90 through 96 for the separation of gutter flash from product P may be utilized. For instance, bi-directional hydraulic actuators 112, 114, 120, and 122 may be ganged and retracted simultaneously, followed by the retraction of ganged actuators 116, 118, 124, and 110 simultaneously. Also, it is permissible to actuate the different pairs of corner actuators, e.g. 112, 114 and 120, 122 or 116, 118 and 124, 110 either simultaneously or serially. In any event, I prefer to not simultaneously retract both actuators connected to any one of the system gutter plate segments, i.e. I do not retract actuator pairs such as 110/112, 114/116, 118/120, or 122/124 simultaneously.

Figures 15, 16, and 17 illustrate three different product wall thickness or interior surface configuration conditions that may be obtained in the region of the product mold cavity parting line perimeter using the apparatus of Figures 1 through 13. Such are achieved using different combinations of the thickness of shim elements 128 placed beneath bronze wear bushings 130 and the different total extent of excess gutter flash receiver elements 98 surface opening area. See Figures 9 and 10. As mentioned above, pivot connections 126 enable gutter plate segments 90, 92, 94 and 96 to move in directions parallel to their pivot axes to change their distances from gutter flash

clamping surface **83** of cap blow-mold sub-assembly **26**. The product uniform wall thickness condition or configuration of Figure 15 is nominally uniform and normally preferred, and the required thickness of shim elements **128** is arrived at during initial set-up trial runs of the invention apparatus rather than by arithmetic calculation. If the localized and thickened wall condition shown in Figure 5 16 is desired, thereby having an essentially convex interior surface configuration, additional thickness of shim elements **128** may be provided or the area extent of adjacent openings of excess gutter flash receiver elements **98** may be reduced. Figure 17 illustrates a thinned product wall thickness condition (concave interior surface configuration) at the product mold-cavity parting line perimeter. Such occurs due to either reduced shim thickness under bronze wear bushing elements **130** or an increased adjacent excess gutter flash accumulator element surface area opening capacity. The thinner product wall thickness is often desired in instances where the product is to have an integrally molded and expandable bellows feature, for instance.

In some blow-molding applications it is desired, because of large product sizes being involved, to remove formed products with partially-attached gutter flash from blow-molding machine 15 **10** as units using overhead take-out conveyor **46** (Figure 1) rather than product conveyor **42** (Figures 2 through 4). In such product applications I utilize the base blow-mold sub-assembly **222** of Figures 18 through 22 in preference to the base blow-mold sub-assembly **22** shown in Figures 5 and 6. The important differences between such sub-assemblies relate to the use of elongated gutter plate segments **290**, **294**, and **296** that each have a relatively-fixed pivot axis **224** positioned near or 20 located at one end, and one bi-directional hydraulic actuator, **110**, **120**, or **122**, pivotally attached to a movable pivot axis at the opposite end. Such an arrangement is sometimes preferred over an arrangement wherein each gutter plate segment has two movable pivot axes with pivotally attached

bi-directional hydraulic actuator components as shown in Figures 5 and 6. Details of fixed pivot 224 and its installation in bronze sleeve bushing 226 in support structure for product mold half 280 are provided in Figure 20. Note that the position of each gutter plate segment 290, 294, and 296 may be translated in directions normal to the plane of the product mold parting line perimeter by 5 longitudinal sliding movement of fixed pivot 224 within and relative to bronze sleeve bushing 226. This allows the thickness of the gutter flash to be adjusted to thereby set a desired wall thickness characteristic at the product mold cavity parting-line perimeter as discussed above.

The apparatus of Figures 18 and 19 also differs from that of Figures 5 and 6 in the use of a different arrangement for actuating gutter flash ejectors. More particularly, and as shown in Figure 10 21 and 22, rather than having an individual bi-directional pneumatic actuator within the gutter plate 20 segments for each gutter flash ejector as in the Figure 5 and 6 scheme, gutter plate segments 290 and 294 each have an internally-located elongated, multi-ramp slide member 226 that is connected to and 25 powered by bi-directional pneumatic actuator 228 mounted on the gutter plate segment and that co- 30 operates with each individual ejector pin 200. (The respective bi-directional actuators for extending 35 and retracting such ejector pins may be mounted on the undersides of the sub-assembly gutter plate 40 segments and received in adjacent recesses in product mold half 280 in the manner disclosed in 45 connection with the crash pad guide pins of the base blow-mold sub-assembly embodiment of Figures 50 34 through 37). Each ejector pin 200 is spring biased to a retracted position by a spring 201 and 55 has one end which engages a ramp 227 in multi-ramp slide member 226 which causes said ejector pin 60 200 to move between a retracted position shown in Figure 21 and an extended position depicted in 65 Figure 22 when bi-directional pneumatic actuator 228 causes slide member 226 to move between its 70 two extreme positions.

As illustrated in Figure 23, the molded product **P** that is produced using sub-assembly 222 retains gutter flash **F** in an attached condition along a very short segment of the product mold parting-line perimeter located adjacent the apparatus uppermost pivots 224. Such enables the product conveyor 46 (Figure 1) to grasp the product and gutter flash combination during each production cycle for discharge through access doors 50, such doors being in an fully-opened condition.

10
15
20
25
30
35
40
45
50
55
60
65
70
75
80
85
90
95

Figures 24 through 28 disclose details of a still different embodiment of the blow-molding apparatus of the present invention - an embodiment that is particularly useful in instances wherein blow-molding machine equipment configuration limitations and product size characteristics preclude the installation and use of a base blow-mold sub-assembly having components such as bi-directional hydraulic actuators projecting outwardly from either side of the sub-assembly. The alternate embodiment is designated 322 in the drawings, and basically is comprised of two end-abutting and pivoted gutter plate segments 390 and 394, a bi-directional dual hydraulic gutter plate segment actuator 350, and interiorly-situated internal cylindrical crash pad elements 370 which are reciprocally powered by bi-directional actuators 374. It should be noted that in this embodiment the crash pads 370 project through the gutter plate segments 390 and 394 but may be retracted so as to not subsequently interfere with the pivoting of those gutter plate segments by operation of dual bi-directional actuator 350. These latter actuator elements may be either conventional hydraulic or pneumatic bi-directional actuators and each is connected to a respective, internally-located and elongated, multi-ramp slide member 326 that co-operates with and reciprocally powers their respective reciprocating crash pad elements 370. To assure complete retraction of the crash pad elements from within their respective gutter plate segment upon withdrawal reciprocation of multi-ramp slide member 326 each crash pad element and 370 is surrounded by a compressed return

compression spring 378. Each multi-ramp slide member 326 is connected to a bi-directional actuator 374 for reciprocal movement between a crash pad element 370 extended position depicted in Figure 25 and a crash pad element 370 retracted position depicted in Figure 26.

Referring to Figures 27 and 28, base blow-mold sub-assembly 322 also includes sets of 5 extensible and retractable bronze wear bushing elements 330 that reciprocate within product mold half 380. Such bushing sets co-operate with and are powered by a respective, internally-located and elongated, multi-ramp slide member 334 which in turn is operationally connected to and powered by a respective bi-directional actuator 376 illustrated only in Figures 24, 27, and 28. As in the case of 10 crash pad elements 370, each bronze wear bushing element 330 also is provided with a surrounding return compression spring 378. Bronze wear bushing elements 330 when extended set the distance between gutter plate segments 390 and 394 and the gutter flash clamping surface of cap blow-mold 15 sub-assembly mold half 381.

It is important to note that excess gutter flash receiver elements 398 which are included in 20 sub-assembly 322 each have an elongated and tapered blind-slot configuration, and together essentially surround, and are uniformly spaced apart from, the peripheral edges or perimeter of product-defining mold cavity 382. Because the configuration of the product P to be molded using sub-assembly 322 has a central bellows section which requires a comparatively thin product wall thickness, the adjacent excess gutter flash receiver elements 398 each include a centrally situated section 398a that has a substantially increased width and that provides additional adjacent excess 25 gutter flash receiver capacity. See the above discussion of Figure 17.

In Figures 29 through 33 I illustrate a blow-mold assembly that may be utilized in the blow-molding machine 10 of Figures 1 through 4 and that is comprised of base blow-mold sub-assembly

422 depicted in Figure 30 and cap blow-mold sub-assembly 426 illustrated in Figure 29. However, rather then be utilized to produce a hollow large, relatively thick-walled thermoplastic resin product, such blow-mold assembly is utilized to form a laminated and contoured product. Such product, also designated as P in Figure 33, is formed from a sheet-like heated parison 440 of thermoplastic resin material and a sheet-like pliable (i.e., compliant) and stretchable mat 442 of densely randomly-oriented and partially-fused thermoplastic resin fibers. (See Figure 31 and 32). The latter material is frequently utilized as a fabric-like surface covering such as in various automotive part applications, e.g. automobile luggage compartment linings, automobile luggage compartment wheel covers, etc.

10
15
20
25
30
35
40
45
50
55
60
65
70
75
80
85
90
95

Cap blow-mold sub-assembly 426 is provided with pivoted and abutting cap gutter plate segments 490a and 494a that each include multiple projecting cleat elements 493 and that each mesh in a unifying sense respectively with gutter plate segments 490b and 494b of base blow-mold sub-assembly 422. Meshing and proper blow-mold sub-assembly alignment upon mold closure is assured by the co-operation of gutter plate segment tapered guide pins 472 with tapered guide pin receptacles 474. Convex projecting cleat elements 493 engage and penetrate into thermoplastic resin mat 442 to retain its edges in a clamped condition during the forming and laminating of product P in the mold assembly fully-closed operating condition.

In the utilization of the blow-mold assembly comprised of sub-assemblies 422 and 426 to produce the laminated product P of Figures 32 and 33, compressed air is introduced into the mold cavity 82 from injection needle 86 only after the after the cap and base blow-mold sub-assemblies 426 and 422 have been operationally closed with parison and matting sheets 440 and 442 clamped between co-operating gutter plate segment 490a, 494a, 490b, and 494b. The injected compressed

air then causes the sheets of material to conform to the configuration of the product cavity in blow-mold half 481 and to become fused together as a rigid lamination.

In Figures 34 through 37 I illustrate certain details of an embodiment 522 of the invention base blow-mold sub-assembly that, although differing from previously disclosed base blow-mold sub-assembly embodiments, may also be advantageously utilized in the production of large, relatively thick-walled blow-molded thermoplastic resin products. The principal differences of this particular base blow-mold sub-assembly embodiment over the previously described embodiments resides in the fact that the included product mold half is comprised of a relatively shallow conventional mold half 580a that is secured to and carried by a relatively deep mold half support 580b, and in the fact that sub-assembly crash pad elements 570 are formed integral with (i.e., comprise a part of) sub-assembly elongate gutter plate segments 590 and 594. Each elongate gutter plate segment has a pair of tapered guide pins 572 which are each connected to and bi-directionally powered by a conventional bi-directional hydraulic or pneumatic actuator 576 that is attached to the underside of the gutter plate segment and that is situated in a recess 578 provided in the adjacent product mold half 580. Each 15 such guide pin co-operates with a tapered guide pin receptacle or receiver 574 provided in the product mold half 581 of the cap blow-mold sub-assembly that co-operates with sub-assembly 522.

See Figure 37. As in the case of other gutter plate segment embodiments, gutter plate segments 590 and 594 each include multiple spaced-apart and gutter flash-penetrating convex cleat insert element 593 and a multiple spaced-apart blind-hole excess gutter flash material receiver element 98. As an 20 alternative, the elongated excess gutter flash receiver elements 398 of the Figures 24 through 28 base blow-mold sub-assembly 322 may be substituted for gutter flash receiver elements 98.

In Figures 38 through 42 I illustrate a further embodiment of the base blow-mold sub-

assembly of the present invention that may be advantageously utilized in the production of large, thick-walled thermoplastic resin blow-molded products. Such base blow-mold sub-assembly is referenced as 622 and includes product mold half 680 with a product cavity 682 having cavity mold parting-line perimeter 708. Surrounding product cavity mold parting-line perimeter 708 are two, elongate gutter plate segments 690 and 692 which are end-abutted, which each have two transversely-movable pivot pins 726 and 728 and which each are supported on wear blocks 732 as shown in Figure 42. Each such elongate gutter plate segment also is provided with elongate excess gutter flash receiver elements 698 and with multiple cleat elements 693.

Sub-assembly 622 differs from previously discussed base blow-mold sub-assemblies in several respects. First, sub-assembly 622 is provided with a gutter plate segment relief or undercut zone 770 which facilitates formation of an gutter flash integral take-out tab that may be used advantageously in connection with blow-molding machine operations that employ overhead take-away conveyors such as 46 of Figure 1. Second, the sub-assembly gutter plate drive is comprised differently than previously discussed gutter plate drives and is located beneath the sub-assembly base plate element 60.

One such gutter plate drive embodiment is illustrated schematically in Figure 40, and a second embodiment is shown schematically in Figure 41. The Figure 40 gutter plate segment drive embodiment is comprised of two, opposite but linearly aligned, double-slotted linear wedge cams 720 and 722 which are each guided linearly by a guide pillar 724 that co-operates with a respective one of wedge cam open-end guide slots 740 or 742, and of two, bi-directional or extendible and retractable actuator devices 610 and 612 that are each connected in driving relation to a respective one of wedge cams 720 and 722. The converging/diverging drive slots 744 and 746 in each wedge

cam engage a respective pivot pin 726 or 728. In the Figure 40 illustration, bi-directional actuator 610 is shown in a retracted condition, and bi-directional actuator 612 is shown in an extended condition. Progressive separation of the integrally attached gutter flash surrounding the blow-molded product is accomplished by the sequential extension of extendible and retractable actuators 610 and 612 whereas in other discussed apparatus embodiments, such as that of Figure 5 and 6, the gutter flash separation is accomplished by actuator device retraction.

In the sub-assembly gutter plate segment drive version of Figure 41, a single pivoted bi-directional or extendible and retractable actuator 610 is advantageously utilized rather than two such devices. In the Figure 41 scheme, linearly bi-directional actuator 610 drives a double-slotted rotary cam 748 which rotates about axis 750. The rotary cam drive slots 752 and 754 each co-operate with a drive pin 756 carried by connector rod 758, and such slots are developed in a manner whereby rotation of rotary cam 748 causes sequential extension movement of co-operating wedge cams 720 and 722. In the Figure 41 illustration, double-slotted wedge cam 722 is shown in its extended condition.

Also, in both versions of base blow-mold sub-assembly 622 the gutter plate drive bi-directional actuator devices or bi-directional actuator device and co-operating rotary cam device are basically located at and secured to the underside of the sub-assembly base plate element 60. Four arcuate guide slots 760 are provided in base plate element 60 and function to guide co-operating pivot pins. See Figure 42. Also, shown in Figure 42 is elongate bronze-like wear plate element 732 which is carried by base plate element 60 to provide wear support for gutter plate segment 692. Since each sub-assembly gutter plate segment is free to be translated relative to and in directions parallel to the longitudinal axes of pivot pins 726 and 728, the position of the gutter plate segment

gutter flash clamping surface relative to the cap blow-mold sub-assembly gutter flash clamping surface may be adjusted to alter product perimeter wall thickness and shape characteristics wall by changing the thickness of wear plate 732 or by changing the thickness of any support shim element provided under that wear plate element. Lastly, the corner filler block 762 which supports transverse 5 gutter flash separator blade 97 may in some applications be advantageously fabricated of a material having low thermal conductivity rather than of metal.

The invention apparatus for separating surrounding integrally-attached gutter flash from a hollow blow-molded product may also be adapted to separate interiorly-situated gutter flash core from the product while the product is retained in its mold cavity. Such is basically accomplished by 10 forming a bellows void in the interiorly-situated gutter flash core using the blow-molding machine compressed air supply, and afterwards progressively collapsing the bellows void using the co-operating interior gutter plate segments provided in the apparatus base blow-mold sub-assembly. The process of collapsing the gutter flash core bellows void causes the interior gutter flash to be progressively separated from the product at its interior mold parting-line perimeter.

15 Figures 43 through 47 schematically disclose details of a blow-mold assembly that is may be operated to progressively separate an interior integrally attached gutter flash core from a blow-molded product while the product is retained in the blow-mold assembly. Such blow-mold assembly is comprised of base blow-mold sub-assembly 822 and cap blow-mold sub-assembly 826 (Figures 46 and 47). Base blow-mold sub-assembly 822 has essentially the same the product cavity, surrounding 20 elongate and pivoted gutter plate segment, and gutter plate segment drive component construction as that described above in connection with base blow-mold sub-assembly 622 and, accordingly, is therefore identified in the drawings by the same reference numeral. However, sub-assembly 822

additionally includes a core gutter plate sub-assembly **922** that is comprised essentially of triangular interior gutter plate segments **990** and **992**, gutter bellows block **932**, and an interior gutter plate segment drive. Each such generally triangular interior gutter plate segment **990** and **992** has two pivot pins, **926** and **928**. In the Figures 43 through 47 base blow-mold sub-assembly **822** scheme, 5 each pivot pin **926** is free to be translated and guided laterally relative to its longitudinal axis during the apparatus core gutter flash separation operation; pivot pins **928** are relatively fixed and remain in their initial position during the gutter flash core separation operation. However, as in the case of base blow-mold sub-assembly **622**, all of the included interior gutter plate segment pivot pins may be provided and operated as translatable pivot pins. Also, interior gutter plate segments **990** and **992** essentially fill the interior open area of base blow-mold sub-assembly mold half **880** in their initial operating condition save for the elongated bellows gap that separates those components and that registers with the gutter flash core bellows void cavity **930** provided in included bellows block **932**.
(See Figure 46).

The gutter plate segment drive provided in sub-assembly 822 to translatably drive pivot pins 926 and pivot their co-operating interior gutter plate segments 990 and 992 about pivot pins 928 is schematically illustrated in Figure 45. Such drive utilizes a single bi-directional (extendible and retractable) actuator device 810 which is coupled to a wedge cam element 934 that includes the integral drive slots 744 and 746 for causing pivotal movement of surrounding elongate gutter plate segments 690 and 692 and also added drive slots 936 and 938 for causing pivotal movement of interior gutter plate segment 990 and 992. Integral drive slots 936 and 938 each co-operate with a pivot pin 926 that projects through a respective arcuate guide slot 940 provided in base plate element 60.

Also, and referring to Figures 46 and 47, cap blow-mold sub-assembly **826** is distinguished from other herein-disclosed cap blow-mold sub-assemblies in that, like sub-assembly **822**, it too includes a gutter flash core bellows void cavity **931**, and that cavity registers with the like cavity **930** of base blow-mold sub-assembly **822**. Cavity **931** basically is situated between the cap blow-mold sub-assembly stepped gutter flash clamping surfaces **83** that extend away from the product mold parting-line perimeter that defines the edge of the desired product interior through-opening area. Further, sub-assembly **826** also includes a conventional air injector needle **86** that is extended into and later retracted from the interior of bellows void formed by cavities **930** and **931**, and that functions to force core gutter flash parison material into complete contact with the surfaces of the co-registered bellows void cavities.

From a method standpoint, and after blow-molding machine **10** drops a heated thermoplastic resin parison to a position between separated blow-mold sub-assemblies **822** and **826** and the blow-mold sub-assemblies are operationally closed, compressed air is injected into the parison interior in parison areas situated in the mold-half product cavity and in the gutter flash core bellows void cavity 15 to expand the parison into contact with the interior surfaces of those cavities. Following product and bellows void formation, exterior gutter plate segments **690** and **692** and interior gutter plate segments **990** and **992** are each pivoted to progressively separate gutter flash from the product along the sub-assembly mold-half product cavity surrounding and interior parting line perimeters. Afterwards the 20 cap and base blow-mold sub-assemblies are operationally opened, and the blow-molded product and the separated surrounding gutter flash and interior gutter flash core are ejected from the blow-mold assembly for subsequent processing.

Various changes may be made to the relative sizes, shapes, materials of construction, and

method or procedural steps specifically described above and detailed in connection with Figures 1 through 47 of the drawings without departing from the intent, meaning, or scope of the claims which follow.

I claim as my invention:

5

卷之三

15